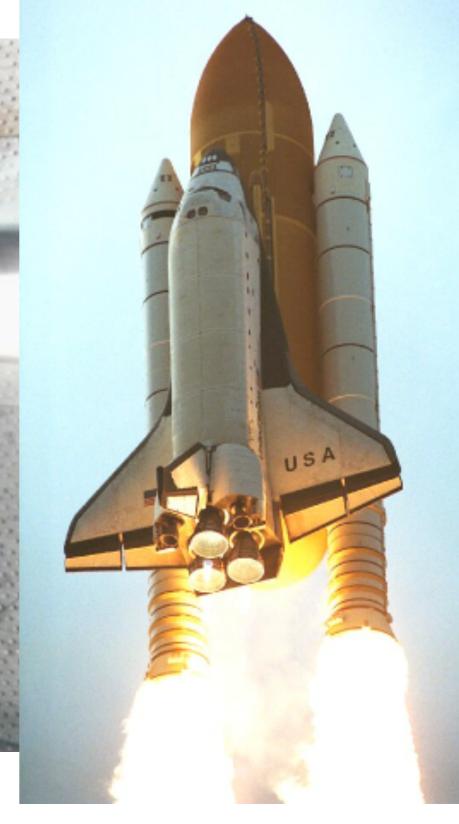


Aerodynamic Tools







Modeling & Simulation

Ground Test

Flight Test

Space Shuttle Program Aerodynamics & Fluid Dynamics

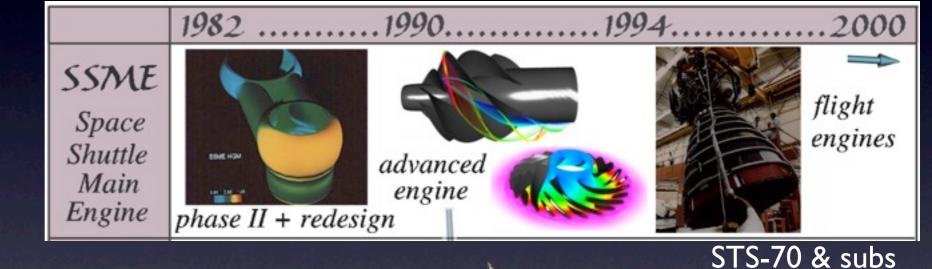
Design Development Operations Retirement

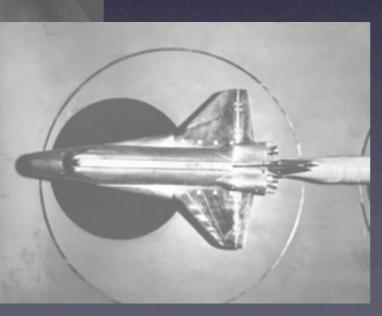
ARC wind tunnel tests Test + CFD FY 2011

44 A/B

176 C/D

1982-present



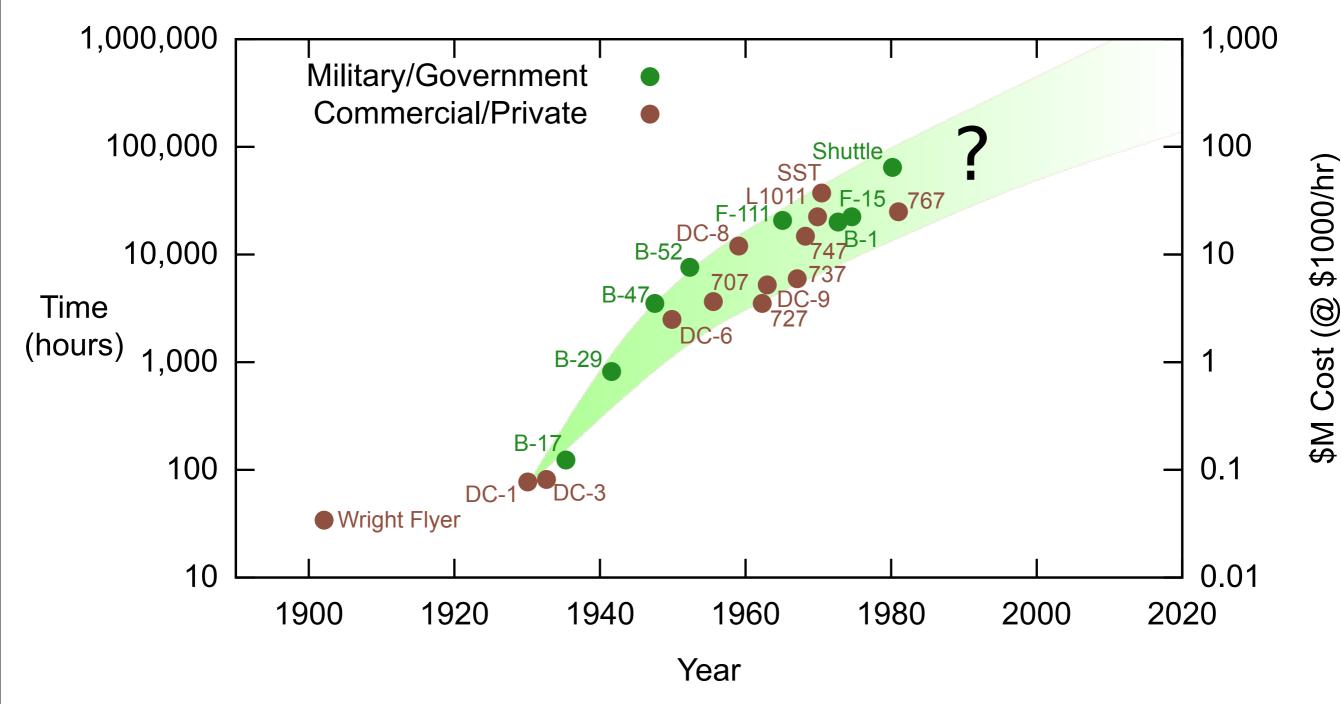




1984 Bancroft & Merritt graphic Cray X-MP solution

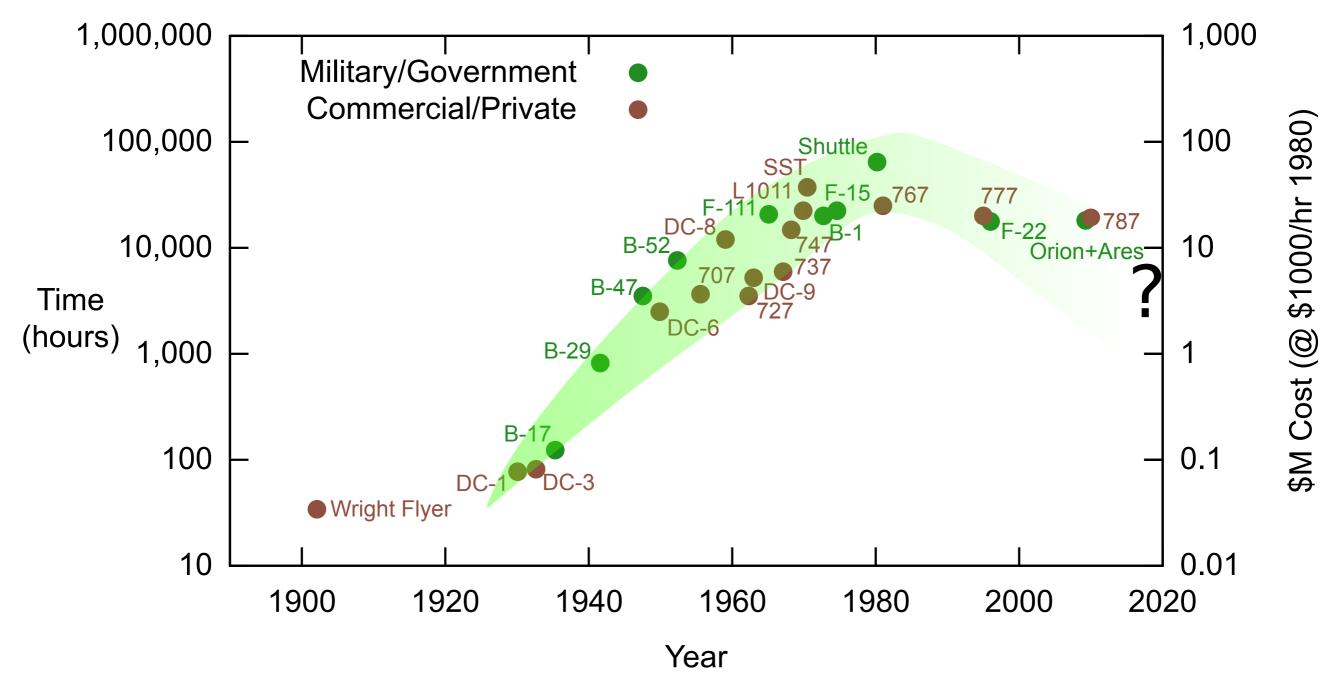
OA-12 / IA9 1973 Unitary Tests

Wind tunnel costs and times dominated aerodynamic database development before 1980.



Data from NASA SP-440 & online sources

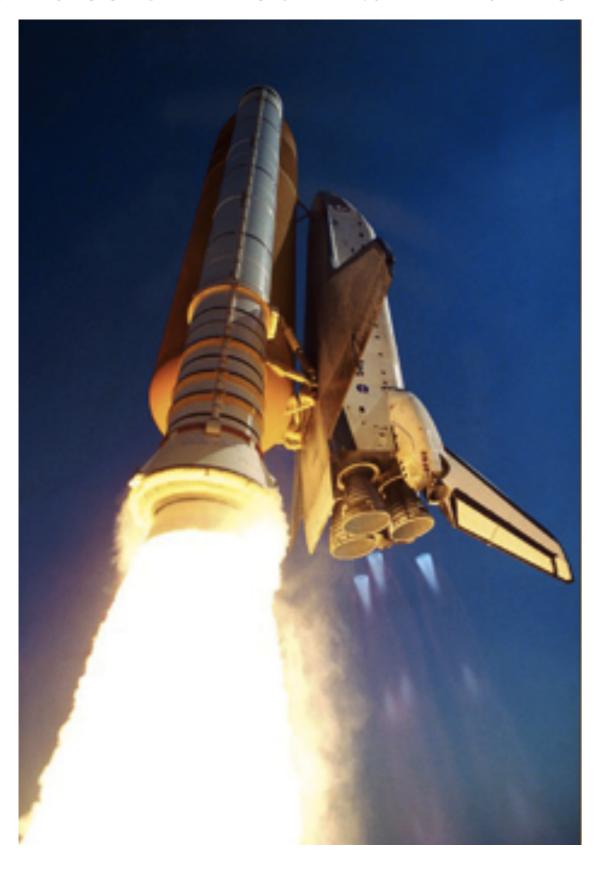
But trends can change ...



Current wind tunnel costs \$3,000 - \$10,000/hour.



Shuttle External Environments



Ground winds
Ignition Over Pressure

▶ 7.8 million lbs thrust

Ascent airloads

▶ Design $\overline{q} = 819 \text{ psf}$

Separation Dynamics

Orbital debris

Hypersonic Entry

▶ 1650 °C/3000 °F

Ground Effects

"Engineering is the art of compromise," Henry Petroski

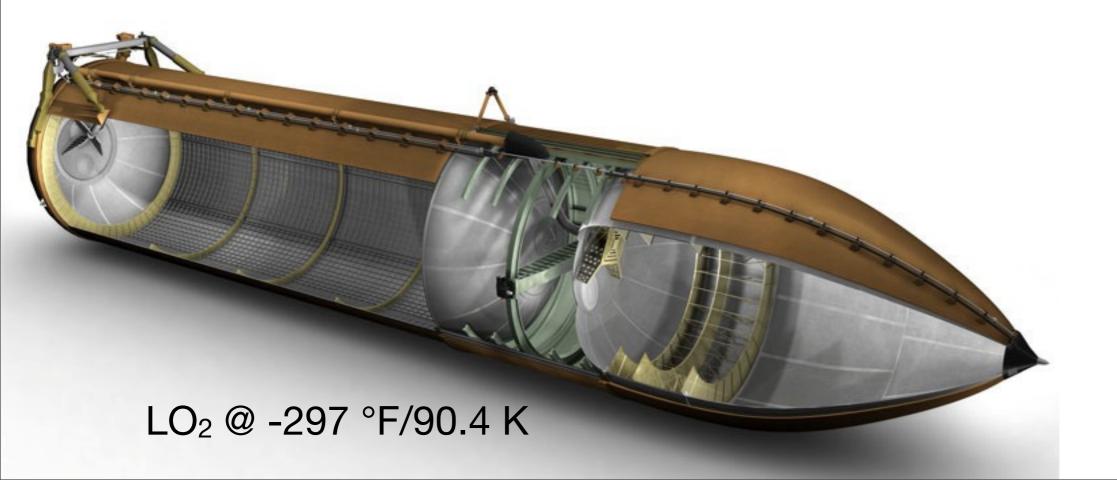
Design goal

Lightest structure that can survive a harsh environment and maximize payload to orbit.

LH₂ @ -423 °F/20.4 K

External Tank

- ▶ 154 ft/47 m long
- ▶ 60,000 lbs empty/1,600,000 lbs filled
- ▶ 27,215 kg empty/725,748 kg filled
- ► Empty/filled = 1/27
- ▶ Typical soda can, I/28, I4 gm/394 gm



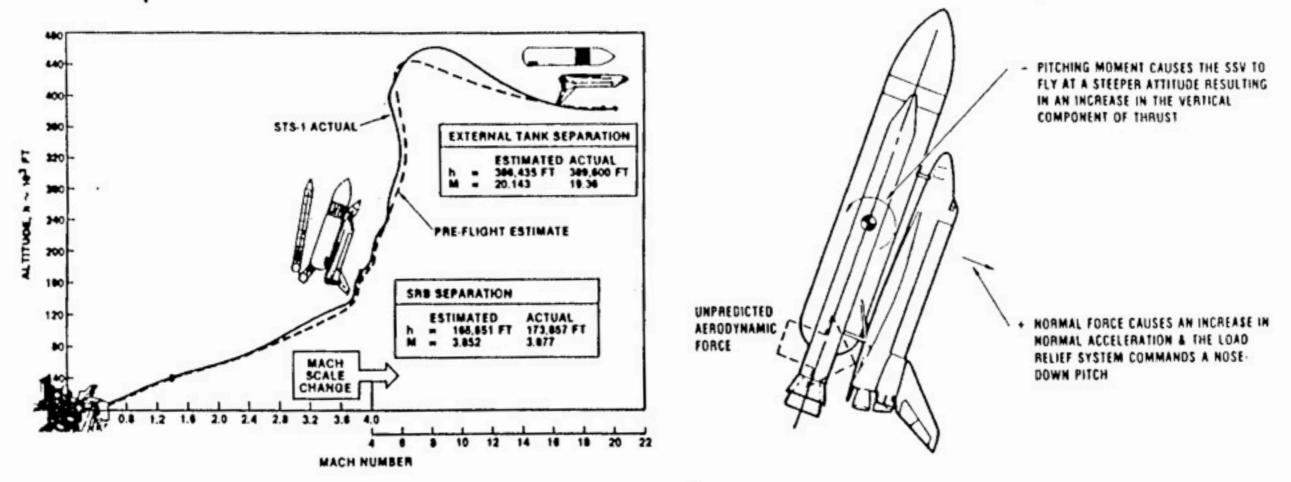
Post Challenger Shuttle Problems

- January 1986 No analytical capability to predict aerodynamics
- 1987 Joseph Steger & Pieter Buning/NASA ARC proposed development of an overset capability to simulate the Shuttle ascent configuration
- Initially focused on fast-separation abort and STS-1 trajectory lofting base pressure issues.
- Payload bay door loads and many more..

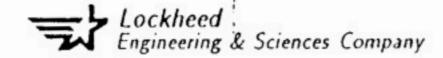
Reference: F.W. Martin, Jr., and J.P. Slotnick, "Flow Computations for the Space Shuttle in Ascent Mode Using Thin-Layer Navier-Stokes Equations," **Applied Computational Aerodynamics**, P.A. Henne, ed., AIAA, 1990, pp. 863-886.

Historical Perspective

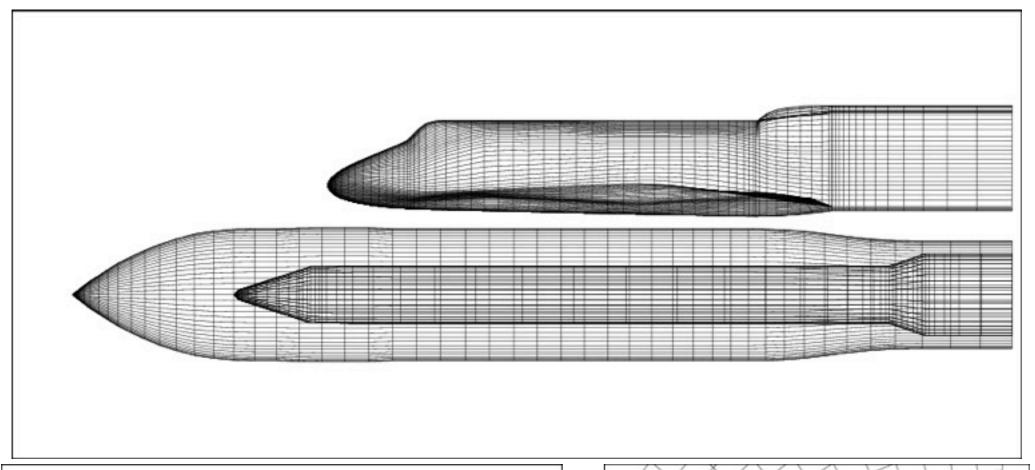
 Discrepancies exist between aerodynamic predictions and flight experience.

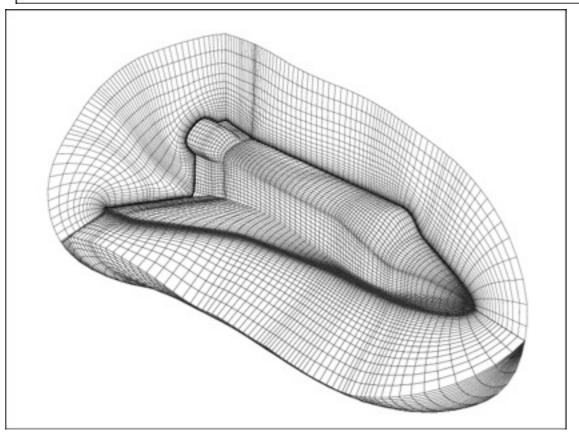


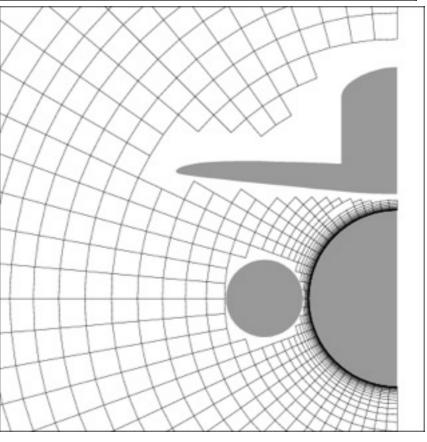
- Force and moment data was easily corrected with flight derived aerodynamic increments.
- Aerodynamic loads (pressure distribution) cannot be readily corrected because of limited flight pressure measurements.



Initial Grid System: 3 grids, 250K points (AIAA-88-4359)

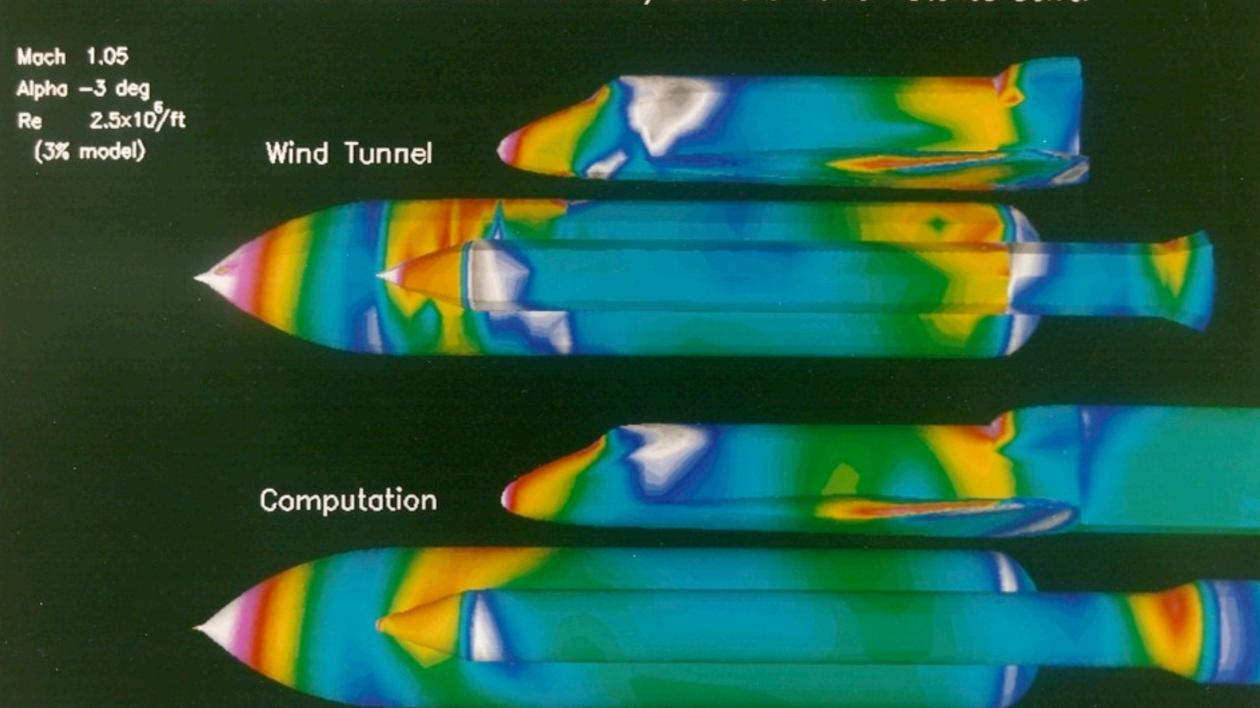




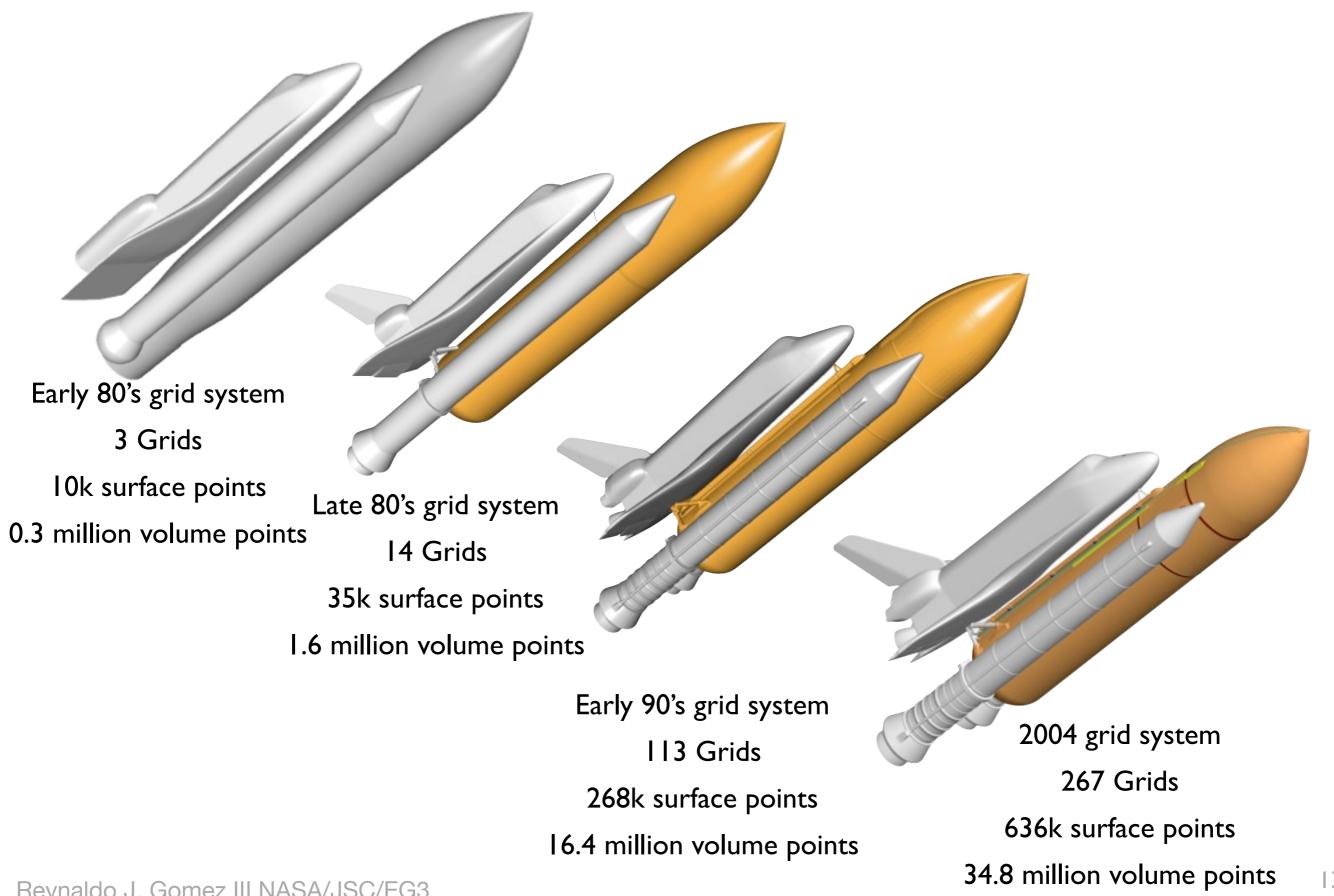


STS ASCENT CONFIGURATION COMPARISON OF PRESSURE COEFFICIENT

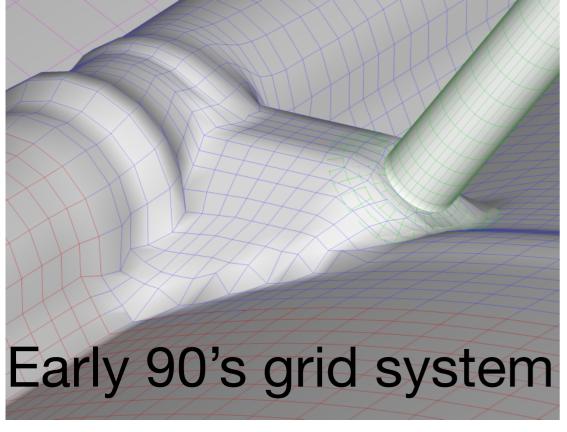
IA105A Wind Tunnel Test with F3D/Chimera Navier-Stokes Solver

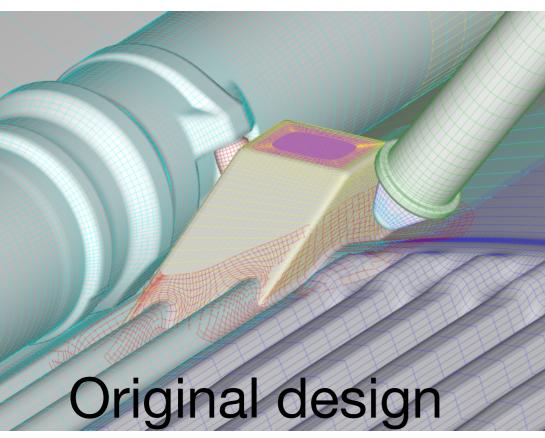


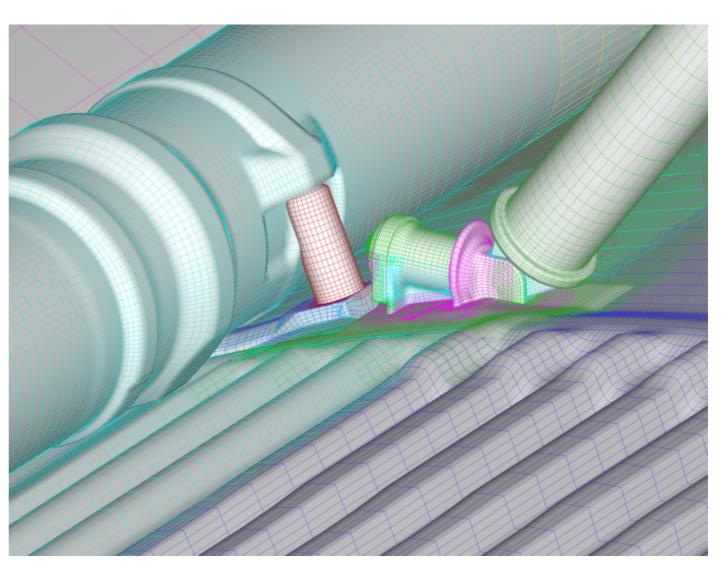
Space Shuttle Launch Vehicle (SSLV) Grid System Evolution



Bipod Ramp Redesign





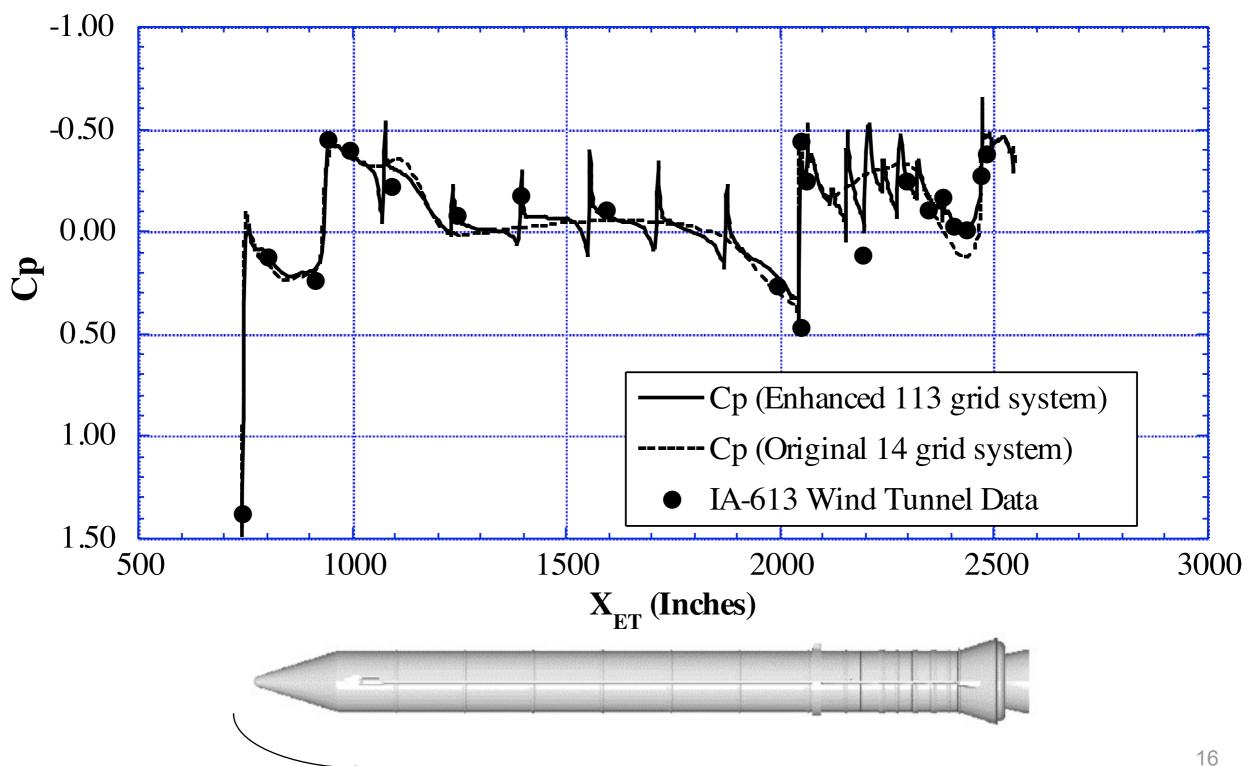


Current configuration



Solid Rocket Booster Surface Pressures

 $\Phi = 0^{\circ}$, Mach 1.25, WT Re((Gomez & Ma, AIAA-94-1859)

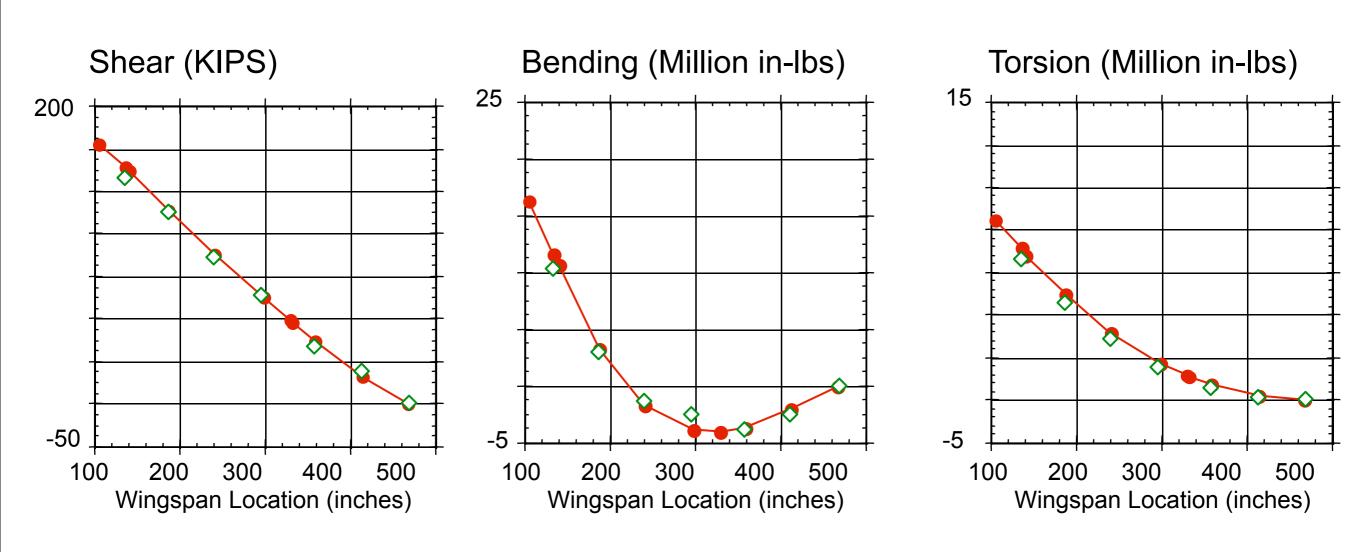


Flight Orbiter Wing Loads (Left Wing)

Mach 1.25, Flight Re

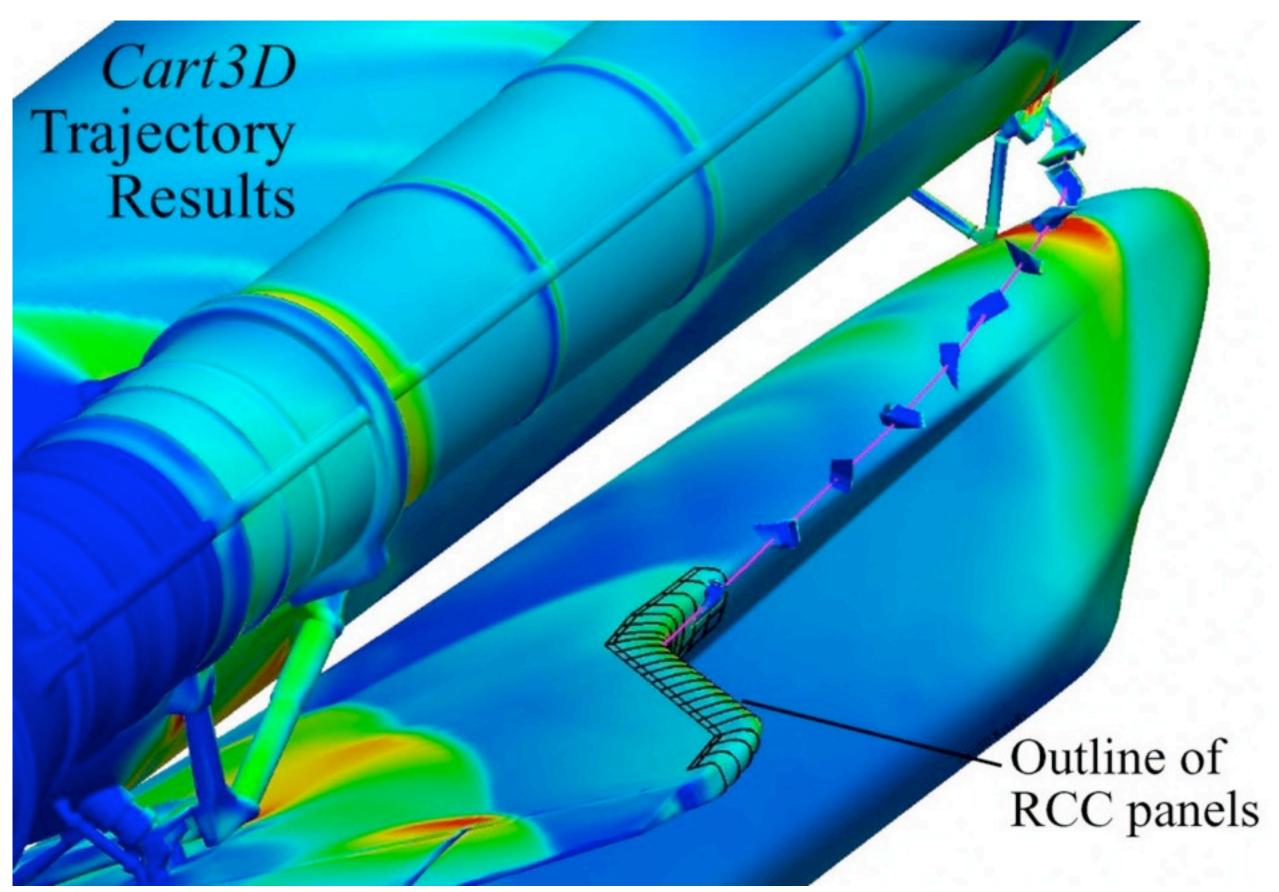
(Slotnick, Kandula, Buning, AIAA-94-1860)





STS-107 Debris

AIAA 2005-1223



The loss of STS-107 initiated an unprecedented detailed review of all external environments.

Ascent airloads, acoustics, heating

Debris liberation, **transport** and capability assessments.

Bipod redesign assessments.

Greatly increased emphasis on verification & validation.

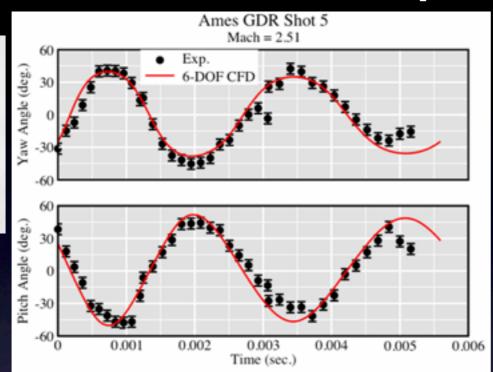
STS-II4 and subsequent missions

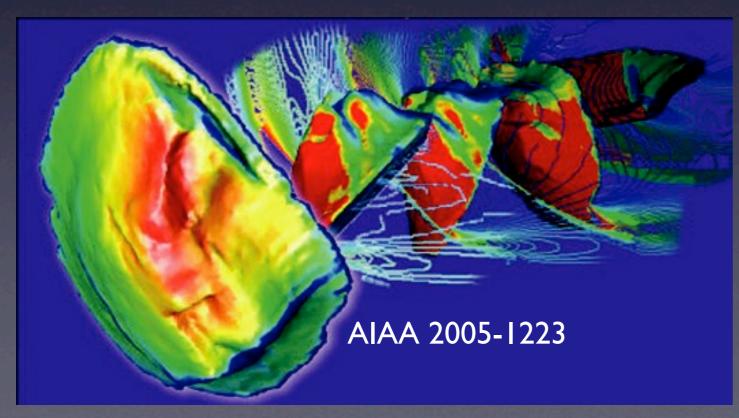
- ▶ PAL ramp foam loss, additional redesign work.
- Prelaunch, inflight and postflight debris transport assessments.

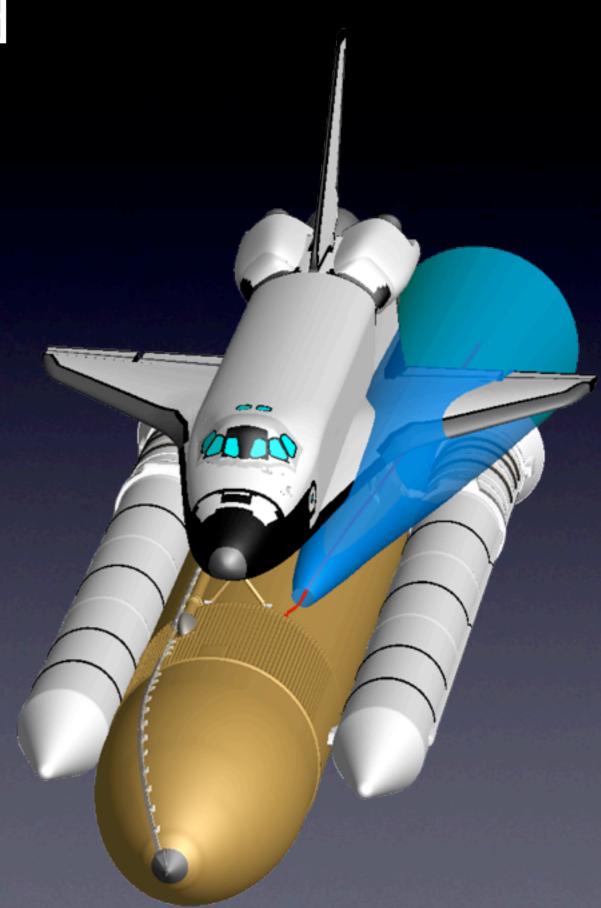
Debris transport aerodynamic models & prediction tools developed



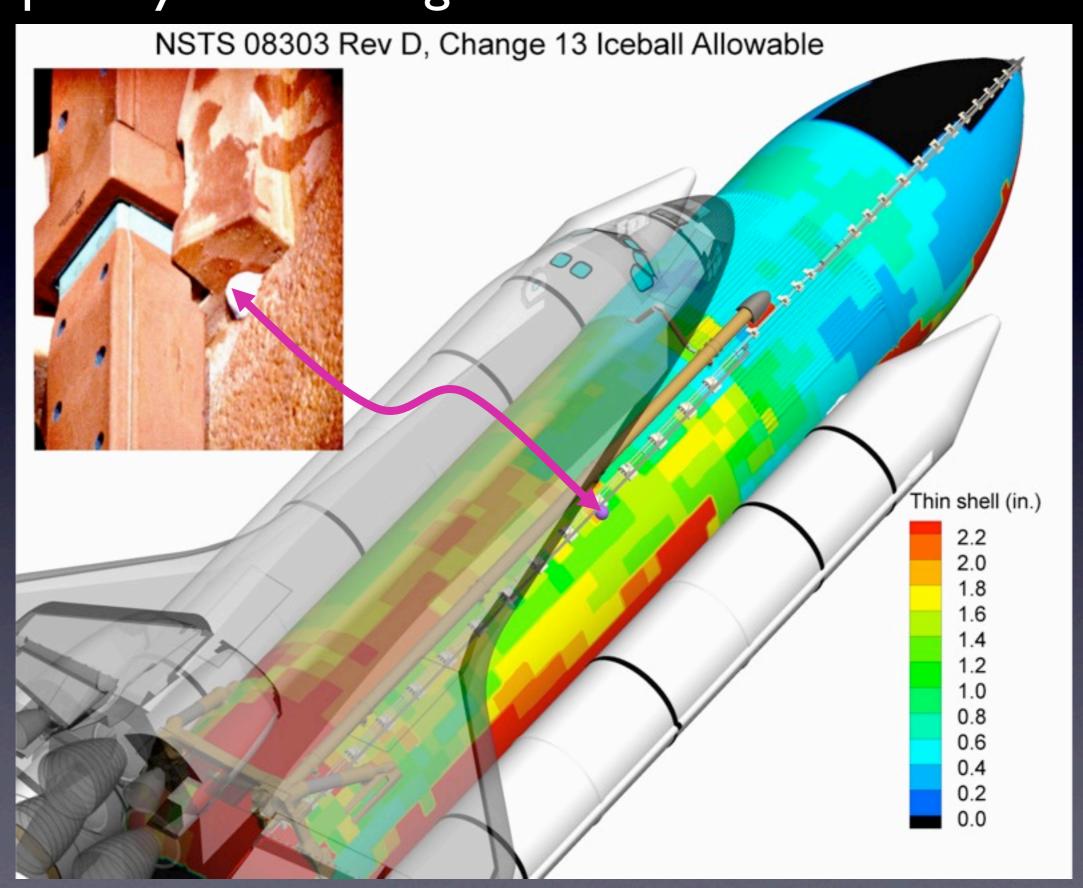
AIAA-2006-0662

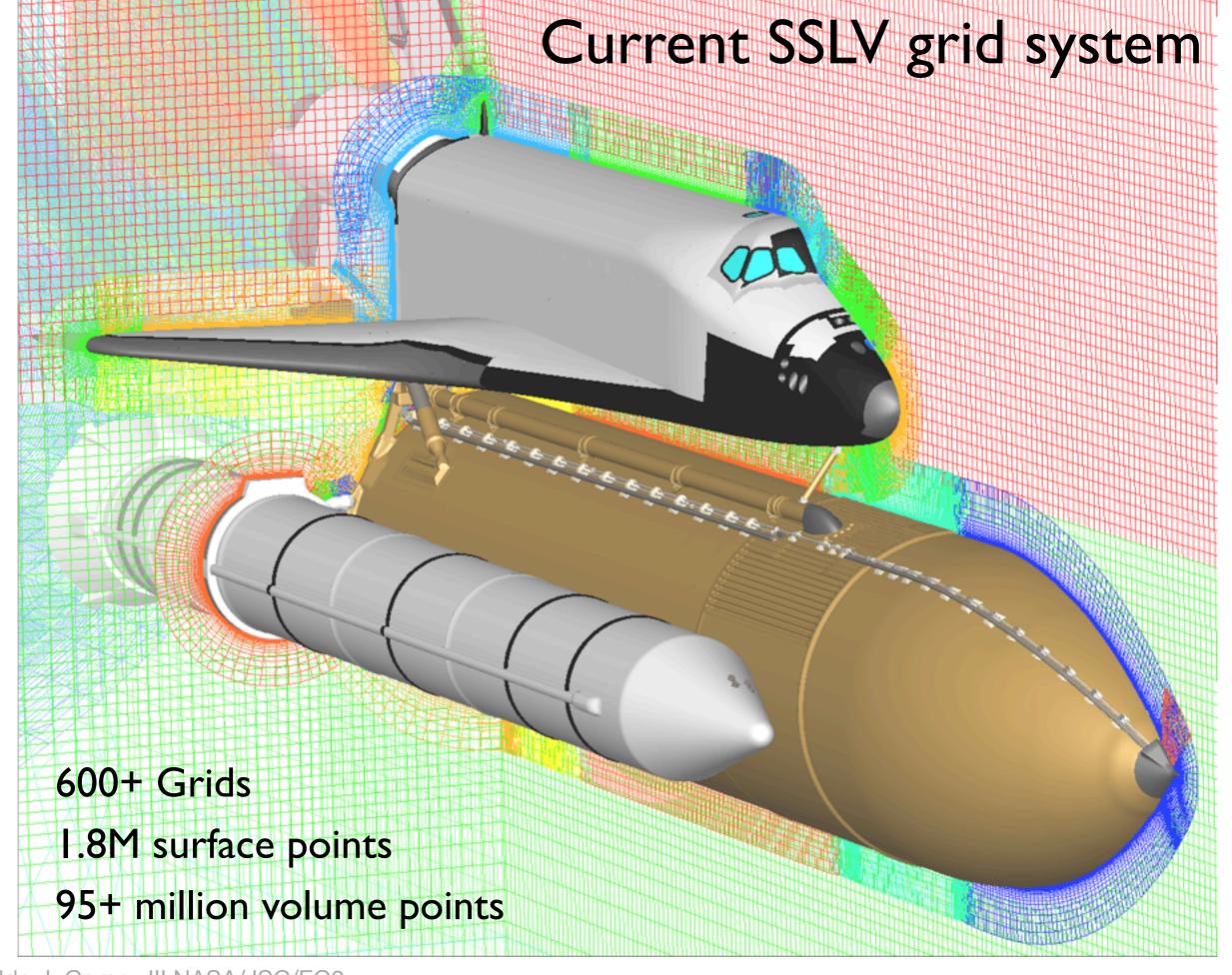




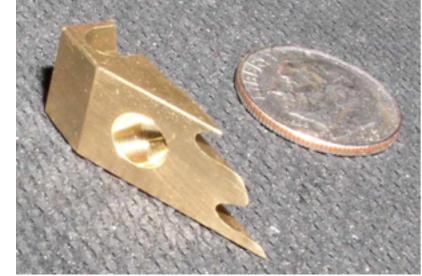


NSTS 08303 day of launch ice ball launch commit tool developed by Stuart Rogers/ARC NAS-07-004

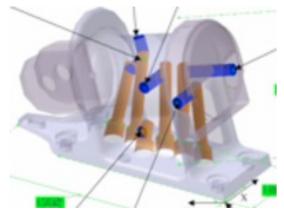


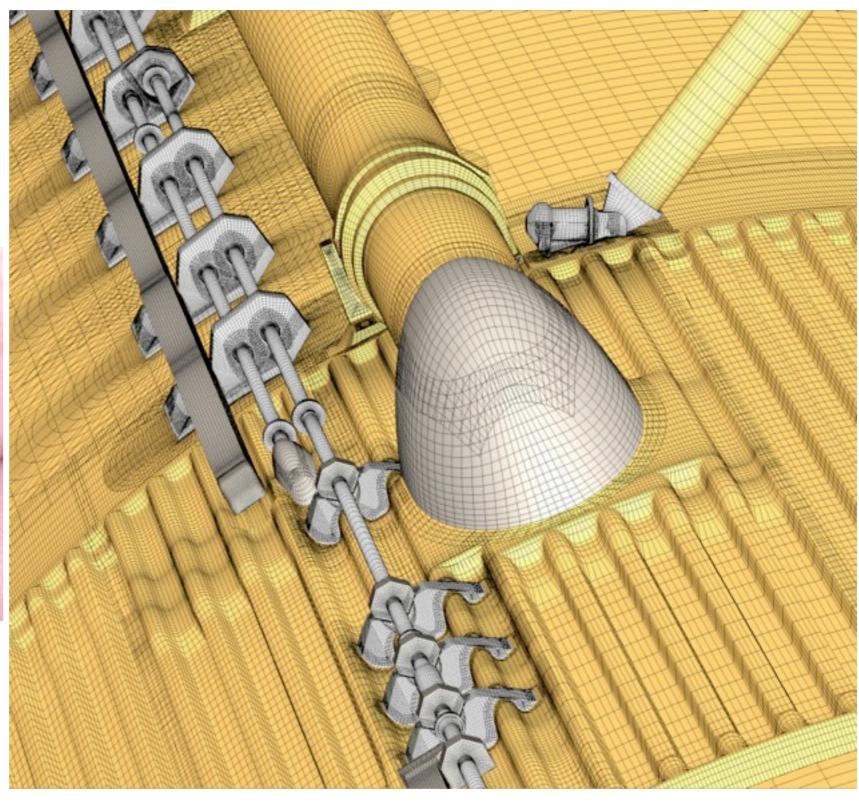


Wind tunnel validation and CFD extrapolation





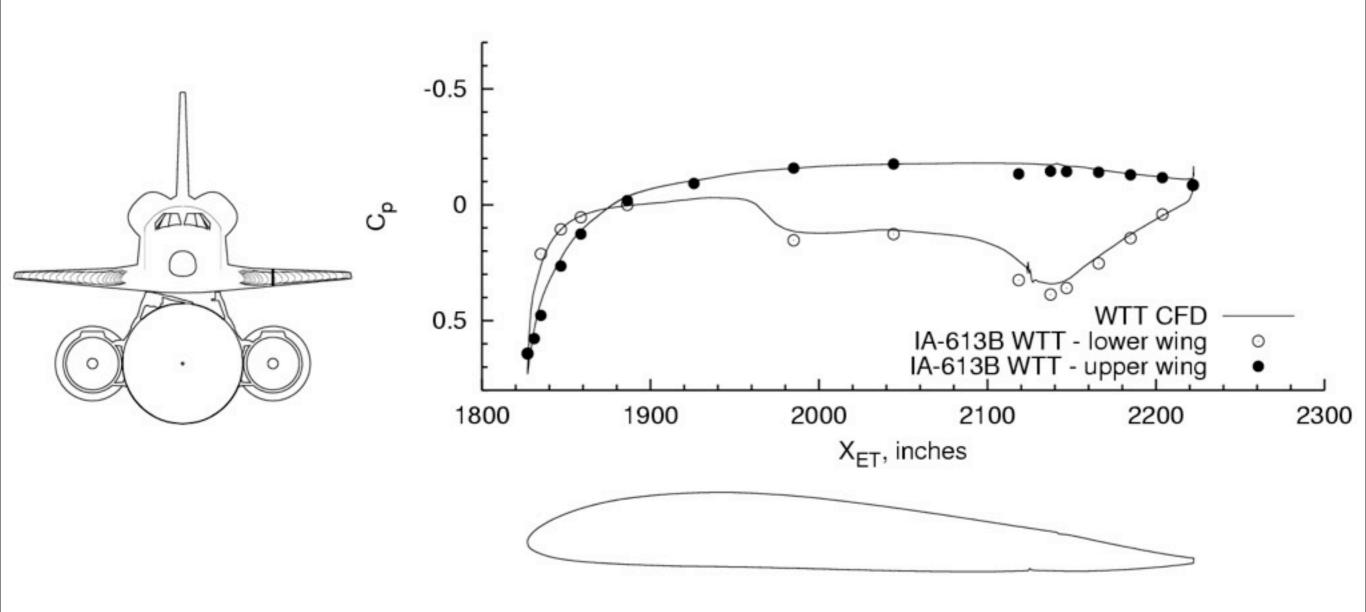




Reynaldo J. Gomez III NASA/JSC/EG3

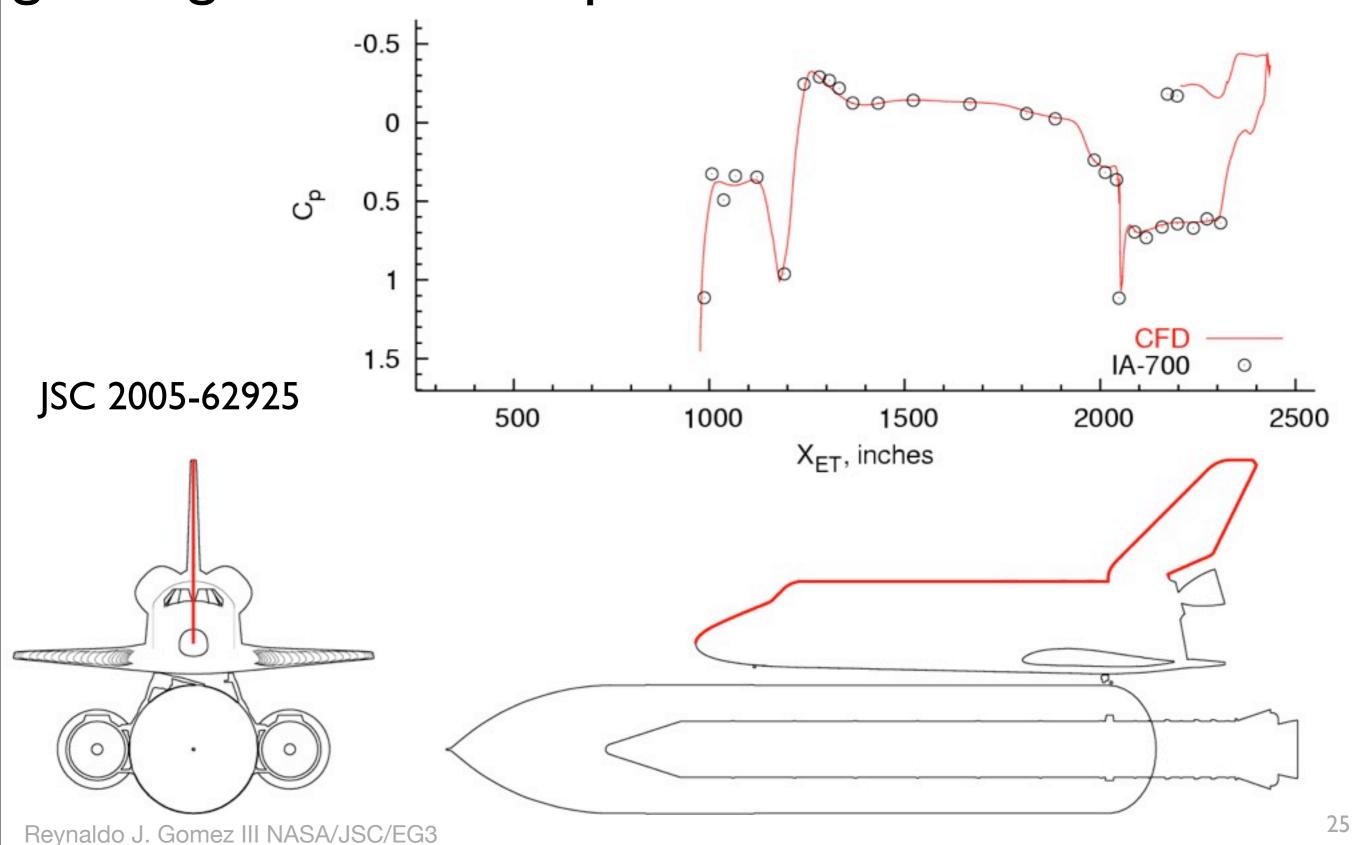
Previous wind tunnel comparisons focused on wing loads.

CFD conditions: $M_{\infty} = 2.50$, $\alpha = 2.03^{\circ}$, $\beta = 0.00^{\circ}$, Reynolds # = 2.50 x10⁶/ft, IB elevon = 4.07°, OB elevon = -4.39° WTT conditions: $M_{\infty} = 2.50$, $\alpha = 2.03^{\circ}$, $\beta = 0.00^{\circ}$, Reynolds # = 2.50 x10⁶/ft, IB elevon = 4.07°, OB elevon = -4.39°

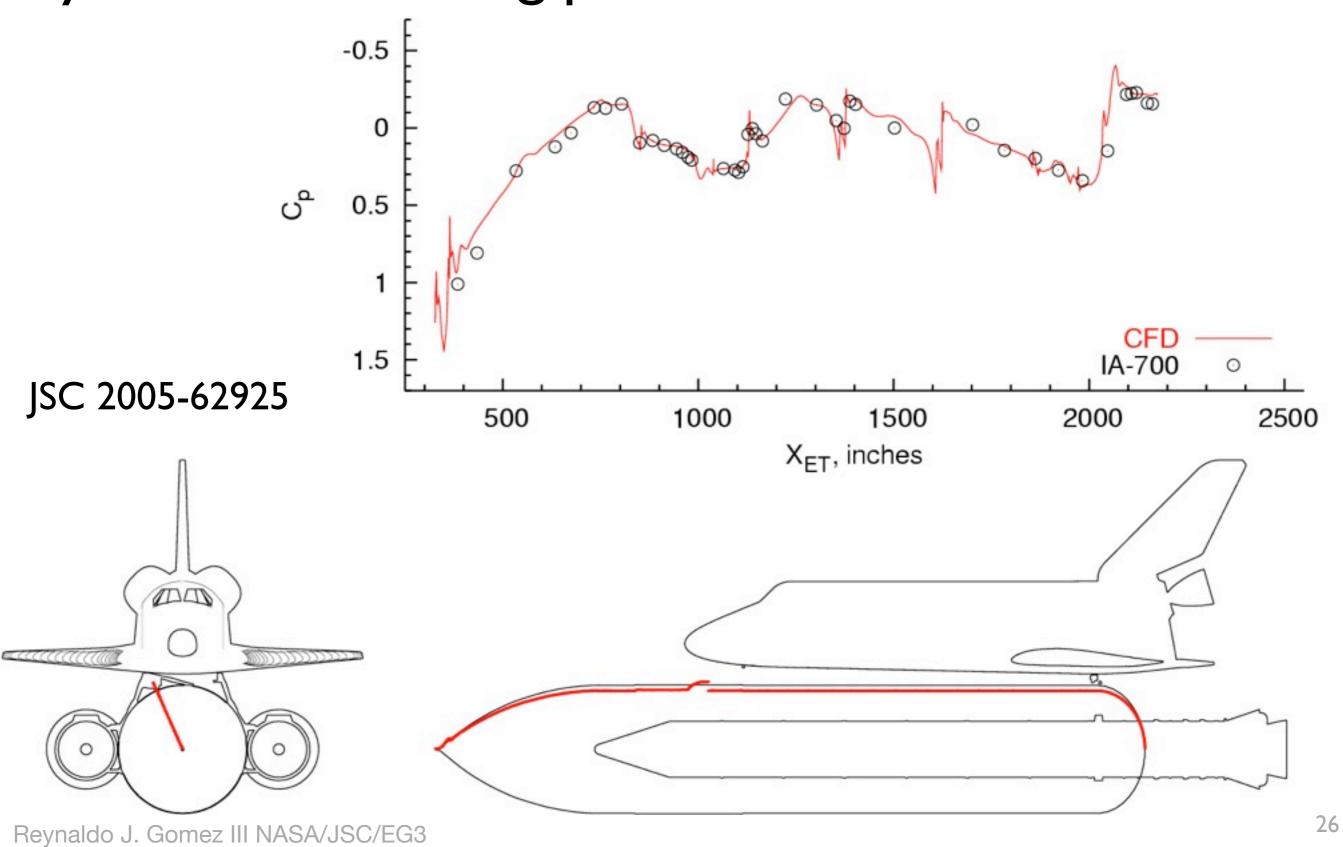


AIAA 2004-2226

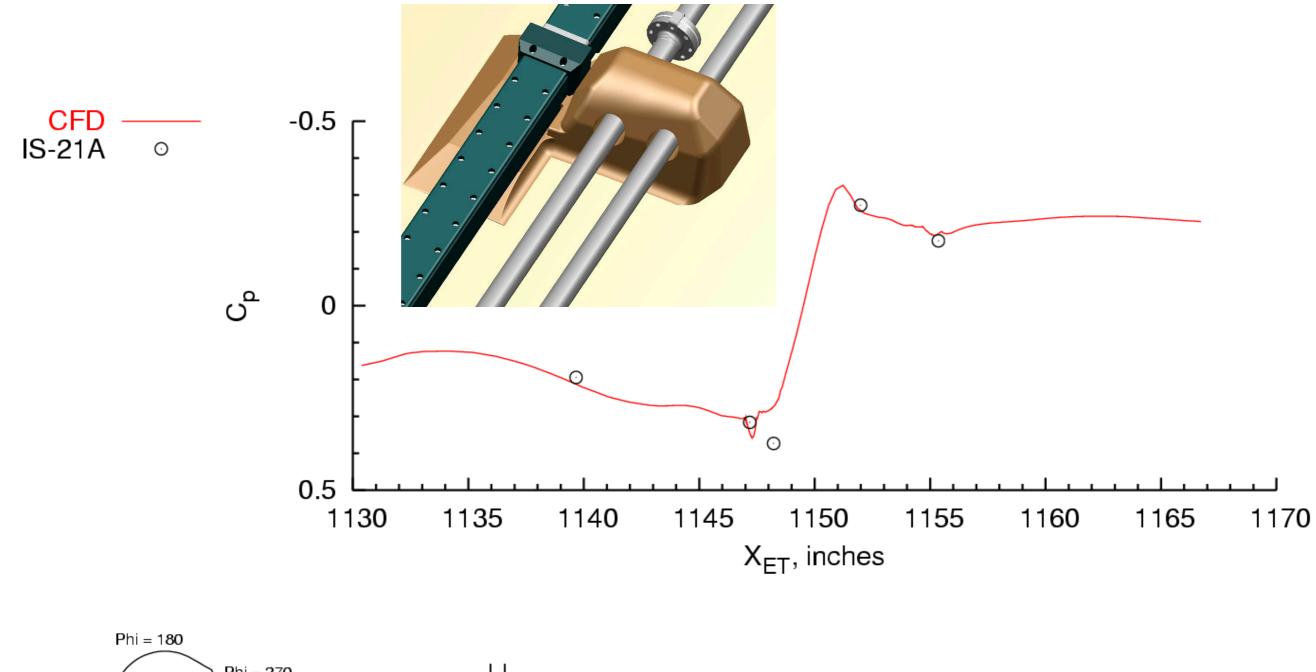
Wind tunnel test pressure comparisons show good agreement with predictions

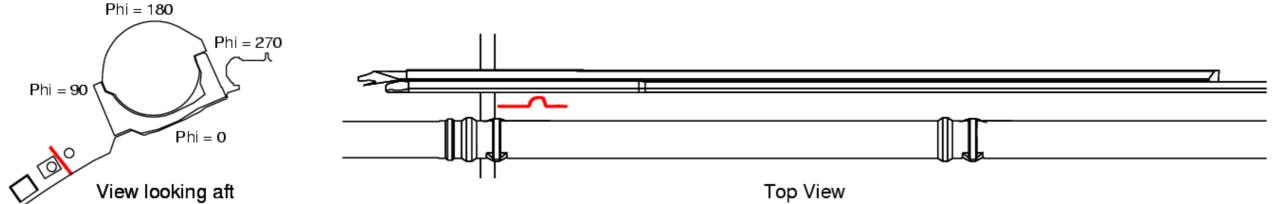


Detailed comparisons along the LO₂ feedline were key to understanding protuberance airloads.



Proposed ice/frost ramp configuration, tested but not flown.

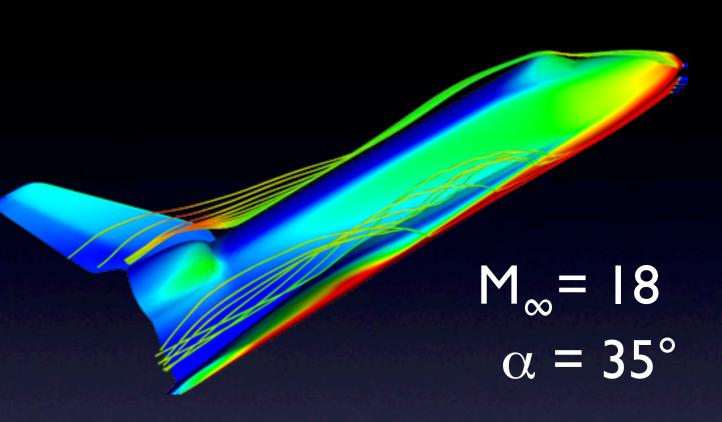


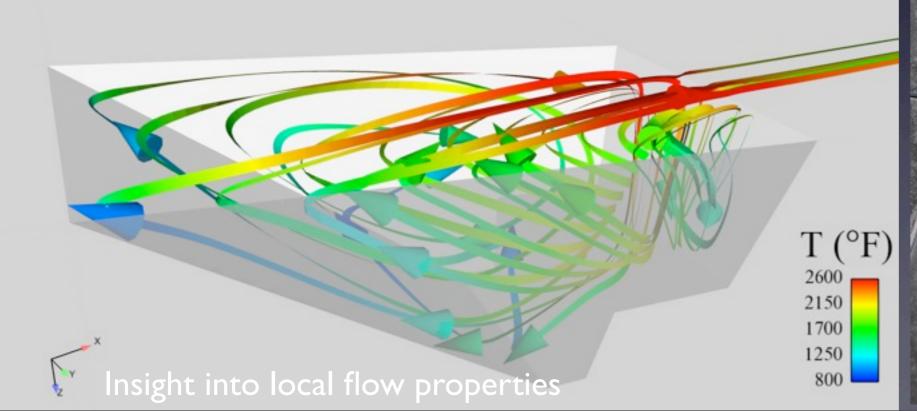


Inflight entry analyses

AIAA 2008-4246



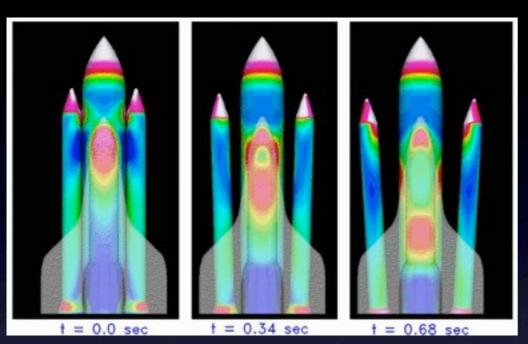






Parallel computing from prelaunch to landing

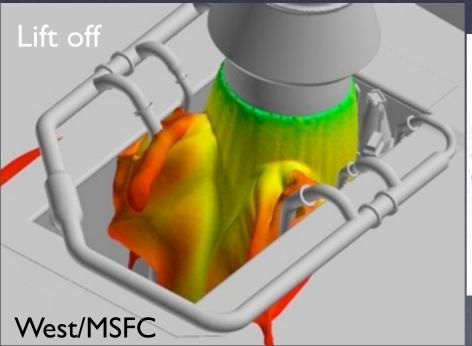
On-orbit Assessments
Hypervelocity Orbital Debris

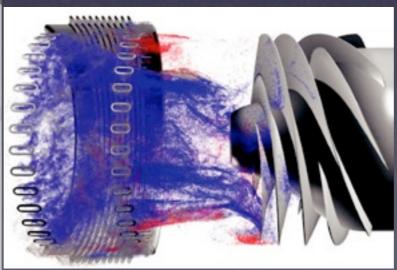




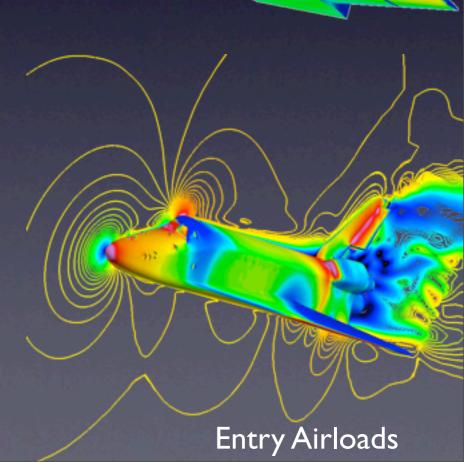


Transonic airloads Roll maneuver

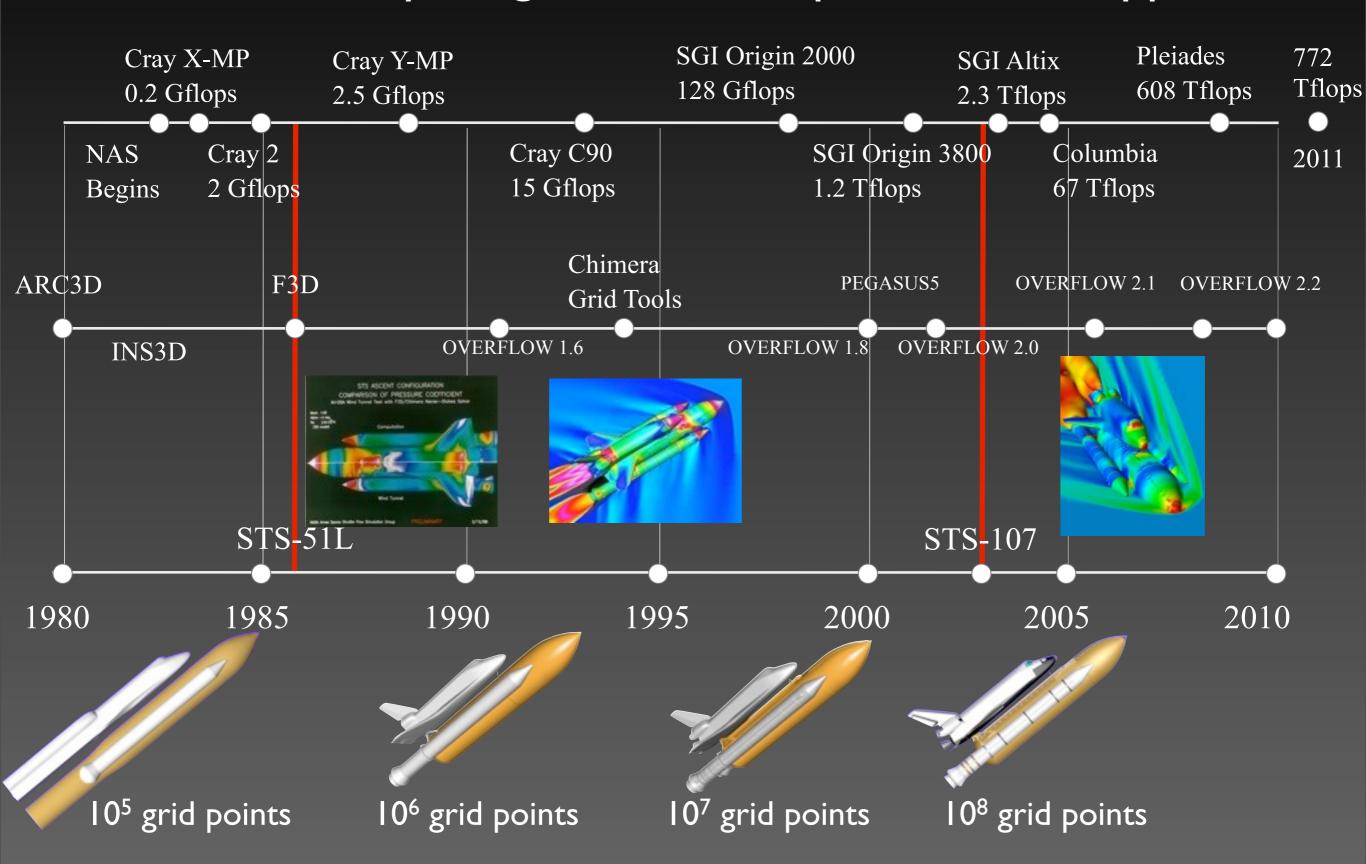




Cetin Kiris/ARC



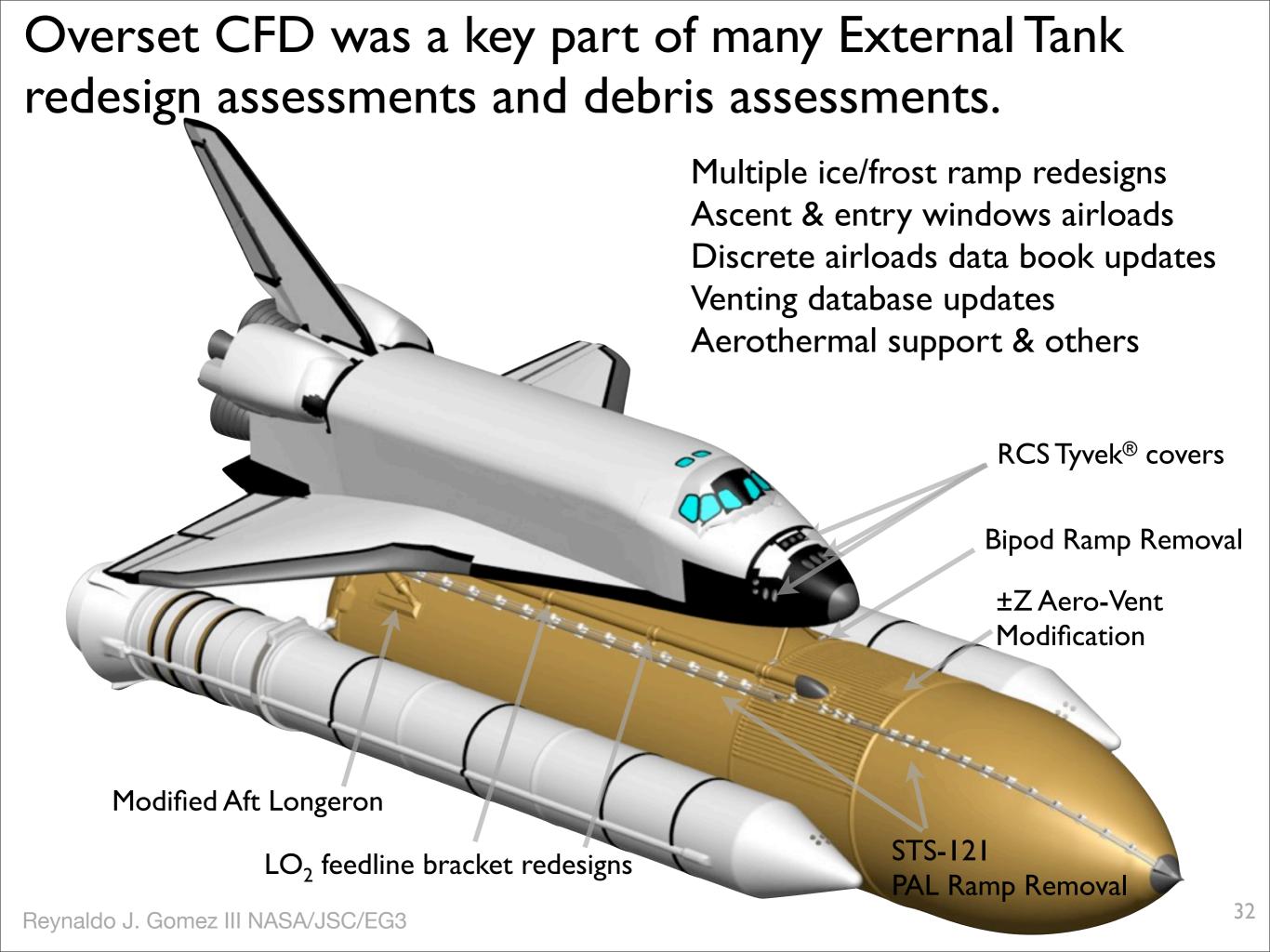
Timeline of Computing & Overset Space Shuttle Applications



We went to the moon without CFD or parallel computers. Why do we need them now?

- Reduce number of physical tests and improve relevance when you run test
 - Nearly 100,000 hours (11 years)
 of Shuttle wind tunnel testing
 - Many facilities have shut down or been mothballed
- Provides flight increments/ environments that cannot be obtained from other sources.





But there is still more work to be done...

STS-134, STS-135?

Some STS-I flight anomalies are still beyond current CFD tool capabilities, e.g.

- Acoustics and heating on complex configurations with strong shock wave-boundary layer interactions
- Physical models (turbulence, chemistry, multiphase flows,...)
 are key limitations that need to be improved.

Future programs will need 10s to 100s of millions of CPU-hours to characterize external environments

 There is evidence that we need 10x more resolution and 10x more solutions than we can currently produce to generate grid converged solutions and populate databases.

